

1 METHOD AND APPARATUS FOR PRODUCING UNIFORM SMALL PORTIONS
2 OF FINE POWDERS AND ARTICLES THEREOF

3 Background of the Invention

4 This invention is directed towards the deposition of small (usually fractional
5 gram) masses on a generally electrically non-conductive substrate. One of the most
6 common methods for accomplishing the goal is practiced by manufacturers of
7 photocopiers and electrophotographic electronic printers. This involves causing
8 charged toner particles to migrate with an electric field to a charged area on a
9 photoreceptor, so-called electrostatic deposition. While electrostatic deposition has
10 been proposed for packaging powdered drugs (see US Patent Nos. 5,669,973 and
11 5,714,007 to Pletcher), electrostatic deposition is limited by the amount of mass that can
12 be deposited in a given area.

13 This limitation is intrinsic to electrostatic deposition technology and is
14 determined by the combination of the amount of charge that can be placed on the
15 photoreceptor and the charge to mass ratio of the toner particles. The mass that can be
16 deposited in an area of a substrate is limited to the charge in the area divided by the
17 charge to mass ratio of the particles being deposited. The maximum amount of charge
18 that can be deposited in an area of a substrate is determined by the substrate electrical
19 properties, the electrical and breakdown properties of the air or gas over it, and by the
20 properties of mechanism used for charging the substrate. Likewise, the minimum
21 charge to mass ratio of particles (which determines the maximum mass that can be

652240 8866260

1 deposited) is determined by the charging mechanism. However, as the charge to mass
2 ratio is decreased, the variation in the charge to mass ratio increases even to the point
3 where some particles may be oppositely charged relative to the desired charge on the
4 particles. This variation prevents the reliable deposition of a controlled mass on the
5 substrate. Furthermore, low charge to mass ratio particles limit the overall speed of
6 deposition because the force of a particle, which sets the particle velocity, from an
7 electrostatic field is proportional to the charge carried by the particle. For these reasons,
8 higher charge to mass ratio particles are generally preferred.

9 Packaged pharmaceutical doses, in the range of 15 to 6000 µg are employed in
10 dry powder inhalers for pulmonary drug delivery. A mean particle diameter of
11 between 0.5 and 6.0 µm is necessary to provide effective deposition within the lung. It
12 is important that the dose be metered to an accuracy of +/- 5%. A production volume
13 of several hundred thousand per hour is required to minimize production costs. High
14 speed weighing machines are generally limited to dose sizes over about 5,000 µg and
15 thus require the active pharmaceutical be diluted with an excipient, such as lactose
16 powder, to increase the total measured mass. This approach is subject to limitations in
17 mixing uniformity and the aspiration of extraneous matter. Hence, electrostatic
18 deposition of such pharmaceutical powders is highly desirable.

19 US Patent 3,997,323, issued to Pressman et al, describes an apparatus for
20 electrostatic printing comprising a corona and electrode ion source, an aerosolized
21 liquid ink particles that are charged by the ions from the ion source, a multi-layered

HAYES, SOLOWAY,
HENNESSEY, GROSSMAN
& HAGE, P.C. 20
175 CANAL STREET
MANCHESTER, NH
03101-2335 U.S.A. 21

603-668-1400

00000000000000000000000000000000

1 aperture interposed between the ion source and the aerosolized ink for modulating the
2 flow of ions (and hence the charge of the ink particles) according to the pattern to be
3 printed. The charged ink particles are accelerated in the direction of the print receiving
4 medium. This patent discusses the advantages in the usage of liquid ink particles as
5 opposed to dry powder particles in the aerosol. However, from this discussion it is
6 apparent, aside from the disadvantages, that dry powder particles may also be used.
7 Furthermore, the charge to mass ratios achieved from using an ion source for charging
8 the powder particles are much higher than those generally achieved using triboelectric
9 charging (commonly used in photocopies and detailed by Pletcher et al in US Patent
10 5,714,007), thereby overcoming the speed issue discussed above. Such printers have
11 been commercially marketed and sold. However, an apparatus for depositing powder
12 on a dielectric (i.e. a powder carrying package) using the Pressman approach also
13 suffers from the above described maximum amount of powder that can be deposited on
14 the dielectric. This is because during the deposition process, charge from both the ions
15 and the charged particles accumulates on the dielectric, ultimately resulting in an
16 electric field that prevents any further deposition. In other words, the amount of
17 material that can be deposited on the dielectric packaging material is limited by the
18 amount of charge that can be displaced across it which is determined by the capacitance
19 of the dielectric and the maximum voltage that can be developed across it.

HAYES, SOLOWAY,
HENNESSEY, GROSSMAN
& HAGE, P.C.
175 CANAL STREET
MANCHESTER, NH
03101-2335 U.S.A.

603-668-1400

SEARCHED SERIALIZED INDEXED

1

SUMMARY OF THE INVENTION

3 The above disadvantages are overcome in the present invention by providing an
4 alternating electric field for depositing particles onto a dielectric substrate. More
5 particularly, the present invention comprises a method and apparatus for depositing
6 particles from an aerosol onto a dielectric substrate wherein the method comprises and
7 the apparatus embodies the following steps: charging the aerosol particles, positioning
8 them in a deposition zone proximate to the dielectric, and applying an alternating field
9 to the deposition zone by which the aerosol particles are removed from the aerosol and
10 deposited on the dielectric substrate thus forming a deposit. The alternating field
11 provides the means to deposit charged particles and/or ions such that the accumulation
12 of charge on the dielectric substrate does not prevent further deposition of particles
13 thus enabling electrostatic deposition of a deposit with relatively high mass.

14 In one embodiment of the invention, the particles are alternately charged in
15 opposite polarities and deposited on the substrate with the alternating electric field,
16 thus preventing charge accumulation on the dielectric substrate.

17 In a second embodiment, an ion source is provided in the deposition zone to
18 provide ions of both polarities for charging the particles. The alternating field
19 determines which polarity of ions is extracted from the ion source. These extracted ions
20 may be used for charging the particles and/or discharging the deposited particles on
21 the dielectric substrate.

HAYES, SOLOWAY,
HENNESSEY, GROSSMAN
& HAGE, P.C.
175 CANAL STREET
MANCHESTER, NH
03101-2335 U.S.A.

603-668-1400

1 In a third embodiment substantially all of the particles are removed from the
2 aerosol. In this embodiment, the mass of the deposit is controlled by measuring the
3 mass flow into the deposition zone and controlling the deposition time to accumulate
4 the desired mass of deposit.

5 In yet another embodiment, the mass of the deposit is determined by measuring
6 the mass flow both into the deposition zone and immediately downstream thereof, and
7 the difference being the amount deposited.

BRIEF DESCRIPTION OF THE DRAWINGS

9 The foregoing and other advantages of the present invention will become
10 apparent from the following description taken together with the accompanying
11 drawings in which:

12 FIG. 1 depicts a schematic cross section of a deposition apparatus made in
13 accordance with the present invention;

14 FIG. 2 illustrates voltage differences in the deposition apparatus of FIG. 1;

15 FIG. 3 depicts an article made in accordance with the present invention; and

16 FIGS. 4 to 7 depict schematic views of various preferred embodiments of the
17 present invention.

DETAILED DESCRIPTION

The present invention provides a method and apparatus for depositing a relatively large mass of material upon a dielectric substrate and the resulting deposition product. The general apparatus for carrying out this deposition is shown in FIG. 1 and

852370 88265260

1 includes a first electrode 5, a dielectric substrate 1 closely proximate to or in contact
2 with a second electrode 3, also herein referred to as a deposition electrode. The volume
3 between the dielectric substrate 1 and the first electrode 5 comprises a deposition zone
4 into which aerosol particles are introduced. This is indicated by the horizontal arrow of
5 FIG. 1. An alternating electric field (the deposition field), indicated by the vertical
6 arrow in FIG. 1 is created within the deposition zone by first electrode 5, second
7 electrode 3 in combination with an alternating voltage source, shown in FIG. 1 as
8 comprising batteries 9 and 11 and switch 7 wherein the polarity of the field generating
9 voltage is determined by the position of switch 7. However, any suitable means for
10 generating an alternating voltage is contemplated to be within the scope of the
11 invention. Charged particles from the aerosol within the deposition zone are
12 electrostatically attracted to the substrate 1 thereby forming a deposit 15 as shown in
13 FIG. 2. The deposit is incrementally formed from groups of particles deposited from
14 each cycle of the alternating field thereby forming a deposit with a relatively larger
15 mass than is possible if a static electric field were to be used. The process of forming the
16 deposit may be terminated by removal of the alternating field. The completed deposit
17 is shown in FIG. 3 as deposited on the dielectric substrate 1.

18 The aerosol particles may comprise a dry powder or droplets of a liquid. In one
19 particular embodiment of this invention, the particles comprise a pharmaceutical, for
20 example, albuterol. The pharmaceutical deposits made from deposited pharmaceutical
21 particles may, for example, form a dosage used in a dry powder inhaler. In a second

HAYES, SOLOWAY,
HENNESSEY, GROSSMAN
& HAGE, P.C. 20
175 CANAL STREET
MANCHESTER, NH
03101-2335 U.S.A. 21

603-668-1400

00221101 00066260

1 embodiment of this invention, the particles comprise a carrier coated with a biologically
2 active agent. An example of a bioactive agent coated carrier is a gold particle (the
3 carrier) coated by fragments of DNA (the bioactive agent). Such particles are used for
4 gene therapy. The prior examples are intended to exemplify the applications of the
5 invention, and not intended to limit the scope of it.

6 The aerosol gas may comprise air or any other suitable gas or gas mixture. For
7 some applications where it is desired to control precisely the environment to which the
8 particles are exposed, and/or to control ion emission characteristics (discussed
9 subsequently), pure nitrogen, or nearly pure nitrogen mixed with a small percentage of
10 another gas, e.g. carbon dioxide, is preferred.

11 Basic components of an aerosol generator include means for continuously
12 metering particles, and means for dispersing the particles to form an aerosol. A number
13 of aerosol generators have been described in the literature and are commercially
14 available. The most common method of dispersing a dry powder to form an aerosol is
15 to feed the powder into a high velocity air stream. Shear forces then break up
16 agglomerated particles. One common powder feed method employs a suction force
17 generated when an air stream is expanded through a venturi to lift particles from a
18 slowly moving substrate. Powder particles are then deagglomerated by the strong
19 shear force encountered as they pass through the venturi. Other methods include
20 fluidized beds containing relatively large balls together with a chain powder feed to the
21 bed, sucking powder from interstices into a metering gear feed, using a metering blade

HAYES, SOLOWAY,
HENNESSEY, GROSSMAN
& HAGE, P.C. 20
175 CANAL STREET
MANCHESTER, NH
03101-2335 U.S.A. 21

603-668-1400

1 to scrape compacted powder into a high velocity air stream, and feeding compacted
2 powder into a rotating brush that carries powder into a high velocity air stream. A
3 Krypton 85 radioactive source may be introduced into the aerosol stream to equilibrate
4 any residual charge on the powder. Alpha particles from the source provide a bipolar
5 source of ions that are attracted to charged powder resulting in the formation of a
6 weakly charged bipolar powder cloud.

7 Non-invasive aerosol concentration (and mass density for aerosols of known
8 particle size and specific density) may be determined optically by using right angle
9 scattering, optical absorption, phase-doppler anemometry, or near forward scattering.
10 A few commercially available instruments permit the simultaneous determination of
11 both concentration and particle size distribution.

12 Particles may be charged within or outside of the deposition zone. One
13 contemplated method of charging particles is triboelectric charging. Triboelectric
14 charging occurs when the particles are made to come in contact with dissimilar
15 materials and may be used with the particles are from a dry powder. Triboelectric
16 charging is well known and widely used as a means to charge toner particles in
17 photocopying and electrophotographic electronic printing processes. Generally,
18 triboelectric charging of particles takes place outside of the deposition zone. A
19 parameter that characterizes the efficacy of particle charging is the charge-to-mass ratio
20 of particles. This parameter is important as it determines the amount of force that can
21 be applied to the particle from an electric field, and therefore, the maximum velocity

1 that particles can achieve during deposition. This, in turn, sets an upper bound to the
2 deposition rate that can be achieved. Charge-to-mass ratios of $1\mu\text{C}$ to $50\mu\text{C}$ per gram
3 are achievable when triboelectrically charging $1\mu\text{m}$ to $10\mu\text{m}$ diameter particles. Such
4 charge-to-mass ratios are documented for pharmaceuticals by Pletcher et al in U.S.
5 Patent 5,714,007. However, other particle charging methods may achieve charge-to-
6 mass ratios at least ten times greater than is possible with triboelectric charging.
7 Accordingly, it is preferred to use such a method to maximize the velocity of the
8 particles when under influence of the deposition field and the rate at which it is possible
9 to form the deposit.

10 Generally these methods for applying higher amounts of charge ~~to~~^t the particles
11 utilize an ion source to generate an abundance of ions of both or either positive and
12 negative polarities. Some of the negative polarity ions may be electrons. As particles
13 from the aerosol pass in front of the ion source (the charging zone), ions of one polarity
14 are accelerated away from the ion source by an electric field through which the particles
15 travel. Ions that impact the particles attach to the particles. Ions continue to impact the
16 particles until the local electric fields from the ions attached to the particles generate a
17 local electric field of sufficient magnitude to repel the oncoming ions. Figures 5 and 6
18 illustrate two approaches for generating charging ions as well as the means for
19 providing an accelerating field.

20 In FIG. 5 ions are generated using corona wire 35. Ions are accelerated through
21 an open mesh screen 39 from an electric field created between open mesh screen 39 and

HAYES, SOLOWAY,
HENNESSEY, GROSSMAN
& HAGE, P.C. 20
175 CANAL STREET
MANCHESTER, NH
03101-2335 U.S.A. 21
—
603-668-1400

603-668-1400

1 electrode 25. Housing 37 may be slightly pressurized to prevent the migration of
2 aerosol particles into the corona cavity. Alternatively, the corona source may consist of
3 one or more corona points at the location of corona wire 35. Aerosol enters the
4 charging zone through channel 23. Particles are charged by corona generated ions that
5 pass through the apertures of screen 39. Such a particle charging method is known. A
6 derivative of this method is described by Pressman et al in US Patent 3,977,323. As
7 shown in FIG. 5, electrode 25 is the previously described deposition electrode and open
8 mesh screen is the first electrode of the previously described deposition zone. Likewise,
9 substrate 33 is the previously described dielectric substrate. Thus, in this exemplary
10 configuration, the charging zone and deposition zone are the same and the particles are
11 simultaneously charged and made to deposit. A particle trajectory is shown by path 41.

12 An alternate particle charging method using an ion source employs a silent
13 electric discharge (SED) charge generator. The construction and operation of this class
14 of device is described by D. Landheer and E.B. Devitts, Photographic Science and
15 Engineering, 27, No. 5, 189-192, September/October, 1993 and also in US Patents
16 4,379,969, 4,514,781, 4,734,722, 4,626,876 and 4,875,060. In the exemplary
17 implementation illustrated in FIG. 6, a cylindrical glass core 43 supports four glass
18 coated tungsten wires 45 equally spaced about its surface. The assembly is closely
19 wound with a fine wire 47 in the form of a spiral. A typical generator unit, available
20 from Delphax Systems, Canton, MA, consists of a 1cm diameter Pyrex glass rod
21 supporting four glass clad 0.018cm diameter tungsten wires. The assembly is spiral

000000000000000000000000

1 wound with 0.005cm diameter tungsten wire at a pitch of about 40 turns per cm. Only
2 one glass coated tungsten wire is activated at any time. The other three wires are spares
3 that may be rotated into the active position if the original active wire becomes
4 contaminated. In FIG. 6, the active wire is that wire closest to the opening in channel
5 23. Ions and electrons are generated in the region adjacent the glass coated wire when a
6 potential of about 2300VACpp at a frequency of about 120 KHz is applied between the
7 tungsten wire core and the spiral wound tungsten wire. Ions and electrons are
8 withdrawn from the active region by an electric field created between spiral winding 47
9 and electrode 25. As in FIG. 5, in the exemplary configuration of FIGS. 6 and 7, the
10 aerosol particles are simultaneously charged and made to deposit.

11 Other ion sources exist that may be suitable for charging particles. For example,
12 it is possible to generate ions with X-rays or other ionizing radiation (e.g. from a
13 radioactive source). When particles are charged with an ion source, any means for
14 making available ions of both or either positive and negative polarity ions is meant to
15 be within the scope of the invention.

16 Another means for charging particles particularly applicable to liquid droplets is
17 described by Kelly in US Patent 4,255,777. In this approach, charged droplets are
18 formed by an electrostatic atomizing device. Although, the charge-to-mass ratio of such
19 particles cited by Kelly is not as high as can be achieved when charging particles with
20 an ion source, it is comparable to that achievable by triboelectric charging and may be

652-2470-0986-6216

1 both preferable in some applications of the invention and is, in any case, suitable for use
2 with the present invention.

3 The above cited configurations are not meant to imply any limitations in
4 configuration. Rather they are meant to serve as examples of possible configurations
5 contemplated by the invention. Therefore, for example, although particle charging with
6 ion sources is shown and discussed wherein particles are charged within the deposition
7 zone, charging of particles with ion sources outside of the deposition zone is also
8 contemplated. All possible combinations of system configuration made possible by the
9 present disclosure are contemplated to be within the scope of the invention.

10 The alternating deposition field preferably has a frequency between 1Hz and
11 10KHz, and most preferably, frequency between 10Hz and 1000Hz, and a magnitude of
12 between 1KV/cm and 10KV/cm. Other frequencies and magnitudes are possible,
13 depending upon the system configuration. For example, a higher deposition field
14 magnitude is possible, generally up to 30KV/cm - the breakdown potential of air and
15 other gases, but not preferred because it may lead to unexpected sparking. Lower
16 deposition field magnitudes are not preferred because the velocity of the aerosol
17 particles in response to the applied field becomes too low. Likewise, an alternating
18 frequency below 1Hz generally is not preferred for most applications because it is
19 anticipated that charge buildup on the dielectric substrate may substantially diminish
20 the magnitude of the deposition field over periods of a second or more. However, there
21 may be applications where this is not the case. Frequencies of 10KHz and higher

HAYES, SOLOWAY,
HENNESSEY, GROSSMAN
& HAGE, P.C. 20
175 CANAL STREET
MANCHESTER, NH
03101-2335 U.S.A. 21

603-668-1400

6524740 2005062600

1 generally are not preferred because it is believed that the charged particles will not have
2 sufficient time to travel through the deposition zone and form the deposition.
3 However, for systems with very small deposition zones, this may not be a factor.

4 The waveform of the deposition field preferably is rectangular. However, it has
5 been found that triangular and sinusoidal waveforms also are effective in forming
6 deposits, although generally less so. The waveform has a duty cycle, which is defined
7 in terms of a preferred field direction. The duty cycle is the percentage of time that the
8 deposition field is in the preferred field direction. The preferred field direction either
9 may be positive or negative with respect to the deposition electrode depending upon
10 the characteristics of a particular system configuration. The duty cycle preferably is
11 greater than 50% and most preferably 90%. The preferred field direction is that which
12 maximizes the deposition rate.

13 As previously described, the deposition field is formed between a first electrode
14 and a second, deposition electrode. The first electrode may or may not be an element of
15 an ion emitter. In some configurations of the invention use of an ion emitter in the
16 deposition zone is advantageous in that it helps to discharge the deposited charged
17 particles thereby preventing the buildup of a field from the deposited charged particles
18 that repels the further deposition of particles from the aerosol. This is particularly
19 advantageous when the duty cycle is greater than 50%. Of course, an ion emitter is
20 required in the deposition zone if the aerosol particles are to be charged within the
21 deposition zone. However, it is also possible to control the charging of the particles,

HAYES, SOLOWAY,
HENNESSEY, GROSSMAN
& HAGE, P.C.
175 CANAL STREET
MANCHESTER, NH
03101-2335 U.S.A.

603-668-1400

656260 805010 020000

1 synchronously with or asynchronously to the alternation of the deposition field such
2 that the buildup of a particle repelling field from the deposit is minimized.

3 The dielectric substrate is closely proximate to and preferably in contact with the
4 deposition electrode. By closely proximate is meant that the separation between the
5 dielectric substrate and the deposition electrode is less than the thickness of the
6 dielectric substrate. In this way, the charged aerosol particles are directed to land on
7 the dielectric substrate in an area determined by the contact or closely proximate area of
8 the deposition electrode. Thus, it is possible to control the location and size of the
9 deposit.

10 The substrate for the deposit may consist of a dielectric material, such as vinyl
11 film, or an electrically conducting material such as aluminum foil. As previously
12 mentioned, as unipolar charged powder is deposited upon the surface of a dielectric, a
13 large electrical potential is formed which generates an electric field that opposes the
14 deposition field and deposition is thus self-limiting at rather low masses. If unipolar
15 charged powder is deposited on the surface of an electrical conductor, then again a
16 surface potential will be built up but of a lower magnitude than that of a corresponding
17 insulating substrate. The ratio of the surface voltage of a deposit on an insulating layer
18 to that of a deposit on the surface of a conducting layer is roughly equal to ratio of the
19 relative thickness of the dielectric plus the thickness of the deposited powder and the
20 thickness of the deposited powder layer. The use of alternating deposition to form

65260 885 6260

1 bipolar layers through the use of ac aerosol charging and ac deposition fields allows
2 larger masses to be deposited onto the surfaces of conductors.

3 The dielectric substrate may be any material and have any structure suitable to
4 its other functions. For example, it may be a packaging medium, such as a tablet,
5 capsule or tablet, or the blister of a plastic or metal foil blister package. The dielectric
6 substrate may also be a pharmaceutical carrier, for example, a pill or capsule. It may be
7 any edible material, including chocolate. Alternatively, it may be simply a carrier of the
8 deposit for carrying it to another location for further processing.

9 We have found with the present invention that it is possible to deposit
10 substantially all of the aerosol particles that pass through the deposition zone under
11 conditions where the flow rate of the aerosol is below a maximum. This maximum flow
12 rate is determined primarily by the magnitude of the deposition field, the charge-to-
13 mass ratio of the charged particles, and their diameters. The capability to deposit
14 substantially all of the aerosol particles has been demonstrated for relatively large mass
15 deposits, much larger than is possible using prior art systems that electrostatically
16 create deposits. For example, we have deposited several milligrams of lactose powder
17 into a blister of a blister pack of 6mm diameter. A particular advantage of the present
18 invention is that there are no limits related to charge-to-mass ratio of the charged
19 particles nor the amount of charge laid down on a substrate as there are with prior art
20 systems. The use of an alternating deposition field enables deposition of charge of
21 either polarity on the combination of substrate and deposit, whether the charge is

HAYES, SOLOWAY,
HENNESSEY, GROSSMAN
& HAGE, P.C. 20
175 CANAL STREET
MANCHESTER, NH
03101-2335 U.S.A. 21

603-668-1400

1 carried by ions or charged particles. The net deposited charge may be therefore
2 neutralized if necessary. As such, the limits to the mass of the deposit become
3 mechanical in nature rather than electrical.

4 The ability to deposit substantially all of the aerosol particles that pass through
5 the deposition zone provides a new method for controlling the mass of the deposit. In
6 this method the mass flow of the aerosol particles that pass into and out of the
7 deposition zone is measured over time by means of sensors 60, 62 located upstream and
8 downstream of the deposition zone. The results could be recorded for manufacturing
9 control records and adjustments in flow rate, etc., made as need be to maintain a
10 desired deposition amount. As previously mentioned there are various known means
11 for measuring the velocity of an aerosol. In combination, these means enable the
12 measurement of the mass flow rate. The integration of the mass flow rate over time
13 gives the total mass. Accordingly, the mass of a deposit may be controlled by
14 measuring the mass flow of aerosol particles into the deposition zone and upon
15 reaching a desired deposit mass, removing the presence of the alternating deposition
16 field. In circumstances wherein a portion of the total aerosol is not deposited as it
17 passes through the deposition zone, a second measuring instrument may be positioned
18 immediately after the deposition zone. The difference between the two measurements
19 represents the total mass deposited from the aerosol as it passes the deposition zone.
20 The deposit may be controlled by removing the presence of the alternating deposition
21 field as described previously. Even in cases wherein substantially all of the aerosol

HAYES, SOLOWAY,
HENNESSEY, GROSSMAN
& HAGE, P.C.
175 CANAL STREET
MANCHESTER, NH
03101-2335 U.S.A.

603-668-1400

1 particles are deposited in the deposition area, the existence of a second measuring
2 instrument provides confirmation of the actual mass deposited, and is of particular
3 interest in applications where the reliability of the mass deposited is of commercial
4 interest such as pharmaceutical dosages. The mass of deposits formed by the present
5 invention is relatively larger than deposits that can be formed with prior art methods
6 that electrostatically create deposits. On the other hand, they may be much smaller
7 than masses conveniently created using prior art methods that mechanically weigh or
8 otherwise mechanically measure or control the mass. As such, the present invention
9 provides a unique means to address a hitherto unaddressed need.

10 The details of the invention may be further examined by considering FIG. 3.
11 Here, an aerosol generator 17 forms an air borne particle dispersion that is carried by
12 enclosed channel 19 to aerosol concentration monitoring station 21. Channel 23 then
13 carries the aerosol through a region where charging device 31 charges the powder. An
14 electrostatic field is provided between the charging device 31 and deposition electrode
15 25. Deposition electrode 25 corresponds to electrode 3 shown in FIG. 1. A dielectric
16 substrate 27 shown here as a blister pack pocket that collects charged particles deflected
17 by the electrostatic field. A second concentration monitoring station 29 is employed to
18 determine how much of the particles have been removed from the aerosol. Under
19 conditions whereby essentially all of the particles are removed from the air stream, this
20 second concentration monitor may not be required. The air stream then moves into

1 collector 30. This collector might consist of a filter or an electrostatic precipitator or
2 both. Alternately, the air may be recirculated through the aerosol generator.

3 EXAMPLE

4 A filling device was set up according to the schematic of FIG. 6. The channel was
5 fabricated of $\frac{1}{4}$ -inch thick polycarbonate sheet. The channel width was 40-mm and its
6 height was 6-mm. A blister pack pocket, formed of 6-mil polyvinyl chloride, having a
7 depth of 4-mm and a diameter of 6-mm was supported on a circular electrode 25 having
8 a diameter of 4-mm.

9 The charge source, consisting of glass core rod 43, spiral wire electrode 47 and
10 four glass coated wire 45 spaced at intervals around the periphery of the core rod, was
11 obtained from Delphax Systems, Canton, MA. Delphax customers employ these rods in
12 discharging (erasing) latent images on Delphax high-speed printer drums.

13 Spiral winding 47 was maintained at ground potential and glass coated tungsten
14 wire 45 was excited using 2300 volt peak-to-peak ac at a frequency of 120 kHz. A Trek
15 high voltage amplifier was employed to provide square wave switching of deposition
16 electrode 25 at a frequency of 35 Hertz. The output voltage was switched between
17 +5kV and -5kV. The duty cycle was set so that negative charges were extracted for 10%
18 of the square wave period leaving positive charge extraction to occur over 90% of the
19 duty cycle.

20 An aerosol consisting of lactose powder, having a particle size in the range of
21 about 3 to about 7 microns, was suspended in a flowing stream of nitrogen gas. The

lactose was aerosolized by the turbulent action of pressurized nitrogen in a Wright Dust Feed aerosolizer manufactured by BGI Inc., Waltham, MA. The aerosol concentration was about 1 microgram/cm³ and the channel flow velocity was adjusted to 30 cm/sec.

Charging and deposition potentials were applied for a period of two minutes during aerosol flow. A well-defined mass of powder, measured and found to be 1 mg, was formed at the bottom of the blister pack pocket. No powder deposition was found at the blister pack walls or on the bottom of the channel.

Subsequent experimental runs established that the mass deposited was proportional to the deposition time over the time intervals of $\frac{1}{2}$ to 5 minutes.

With the present invention, it is also possible to multiplex the operation of two or more deposition zones served from a single aerosol source by configuring deposition zones along the aerosol path and selectively applying an alternating deposition field at one deposition zone at a time. Aerosol particles passing into a deposition zone where no alternating deposition field exists simply pass through the deposition zone whereupon they can pass into a next deposition zone.

16 Although various embodiments which incorporate the teachings of the present
17 invention have been shown and described in detail herein, many other varied
18 embodiments that still incorporate these teachings may be made without departing
19 from the spirit and scope of the present invention. For example, the aerosol particles
MAN
20 may comprise carrier particles which may comprise inert substrates including
ET
21 biocompatible metal particles coated with a bioactive agent.

HAYES, SOLOWAY,
HENNESSEY, GROSSMAN
& HAGE, P.C. 20
175 CANAL STREET
MANCHESTER, NH
03101-2335 U.S.A. 21